

WellSharp Subsea Baker #1

Hole Dimensions		
Depth (MD/TVD)	11,090	feet
9 5/8" Casing shoe	7,800	feet
Hole size	8 1/2	inch
Current mud weight	13.5	ppg
Air gap	80	feet
Water depth	740	feet
Internal Capacities		
6 1/2" Drill collars (length 900 feet)	0.00768	bbl/foot
5" Drill pipe - capacity	0.01776	bbl/foot
5" Drill pipe - metal displacement	0.00650	bbl/foot
5" Drill pipe- closed end displacement	0.02426	bbl/foot
Choke line	0.006	bbl/foot
Marine riser	0.39	bbl/foot
Annular Capacities		
Open hole / Drill collar	0.0292	bbl/foot
Open hole / Drill pipe	0.0459	bbl/foot
Casing / Drill pipe	0.0505	bbl/foot
LOT		
Shoe test mud weight	12	ppg
Leak off pressure	2725	psi
Pump Details		
Pump output	0.109	bbl/stk
SCR pressure up Riser at 40 SPM	550	psi
Choke line friction at 40 SPM	300	psi
Shut in data		
SIDPP	200	psi
SICP	600	psi
Pit gain	12	bbls

Note: If Riser or Choke Line length are not given, then their length will be Air Gap + Water Depth.



Valued Quality. Delivered.

Well Name:
Subsea Baker #1

Date:

Well Info:

- A. Hole TVD
11090
- B. Current MW ppg
13.5
- C. Slow Pump Pressure
550
- D. Slow Pump SPM
40

Kick Info:

- E. (SIDP)
200
- F. (SICP)
600
- G. Pit Gain bbls
12

KWM = (SIDP ÷ .052 ÷ TVD) + Current Mud Weight

$$\left(\frac{\text{(E)}}{\text{(A)}} \div .052 \div \frac{\text{(B)}}{\text{(C)}} \right) + \frac{\text{(B)}}{\text{(C)}} = \text{Round up KWM}$$

$$\left(\frac{200}{11090} \div .052 \div \frac{13.5}{550} \right) + \frac{13.5}{550} = \boxed{13.9}$$

ICP = Slow Pump Pressure + SIDP

$$\frac{\text{(C)}}{\text{(E)}} + \frac{\text{(B)}}{\text{(C)}} = \text{ICP}$$

$$\frac{550}{550} + \frac{200}{550} = \boxed{750}$$

FCP = KWM ÷ CMW x Slow Pump Pressure

$$\frac{\text{(KWM)}}{\text{(B)}} \times \frac{\text{(C)}}{\text{(C)}} = \text{FCP}$$

$$\frac{13.9}{13.5} \times \frac{550}{550} = \boxed{567}$$

Stks to Bit ÷ 10 = **172** stks

Strokes to Bit ▶

	Strokes	Pressure
	0	750
(1)	172	732
(2)	344	714
(3)	516	696
(4)	688	678
(5)	860	660
(6)	1032	642
(7)	1204	624
(8)	1376	606
(9)	1548	588
(10)	1723	567

◀ ICP

18 psi
(ICP - FCP) ÷ 10 =

◀ FCP

Shoe Pressures:

- H. Shoe TVD
7800
- I. LOT Pressure
2725
- J. Test MW
12.0
- K. Frac. Gradient

$$\left(\frac{\text{(I)}}{\text{LOT}} \div .052 \div \frac{\text{(H)}}{\text{Shoe TVD}} \right) + \frac{\text{(J)}}{\text{TMW}} = \text{Round down MAMW}$$

$$\left(\frac{2725}{2725} \div .052 \div \frac{7800}{7800} \right) + \frac{12.0}{12.0} = \boxed{18.7}$$

Or

Or

$$\frac{\text{(I)}}{\text{Frac. G. (K)}} \div .052 =$$

$$\left(\frac{\text{(MAMW)}}{\text{(MAMW)}} - \frac{\text{(B)}}{\text{CMW}} \times .052 \times \frac{\text{(H)}}{\text{Shoe TVD}} \right) = \frac{\text{(I)}}{\text{LOT}} = \text{MASP before kick with Current MW}$$

$$\left(\frac{18.7}{18.7} - \frac{13.5}{13.5} \times .052 \times \frac{7800}{7800} \right) = \frac{2725}{2725} = \text{MASP before kick with Current MW}$$

$$\left(\frac{\text{(MAMW)}}{\text{(MAMW)}} - \frac{\text{(KWM)}}{\text{CMW}} \times .052 \times \frac{\text{(H)}}{\text{Shoe TVD}} \right) = \frac{\text{(I)}}{\text{LOT}} = \text{MASP after kill with Kill MW}$$

$$\left(\frac{18.7}{18.7} - \frac{13.9}{13.5} \times .052 \times \frac{7800}{7800} \right) = \frac{2725}{2725} = \text{MASP after kill with Kill MW}$$

Volume Info:	Drillstring Volume (surface to bit)	Miscellaneous Calculations:
a) Hole MD 11090	(1) Length (ft) 10190 x Internal Capacity 0.01776 = 180.97 +	Pressure drop per step (one-tenth of strokes to bit): $(ICP - FCP) \div 10 =$ 18
b) Shoe MD 7800	(2) 900 x 0.00768 = 6.91 +	Pressure drop per 100 strokes to bit: $(ICP - FCP) \times 100 \div \text{Strokes to Bit} =$ 10
c) Pump Output (bbls/stk) 0.109	(3) <input type="text"/> x <input type="text"/> = <input type="text"/> +	(Subsea) Dynamic (adjusted) casing pressure after pump start-up: $(SICP - CLF) =$ 300
d) Choke Line Length 820	(4) <input type="text"/> x <input type="text"/> = <input type="text"/> +	
e) Riser Length 820	Total Drillstring Volume 187.88 \div 0.109 (c) = 1724 Strokes Surface to Bit	
f) DC Length 900		

Annular Volumes and Strokes

(Subsea only) (e) $\left\{ \begin{array}{l} \text{Choke Line Capacity} \\ \text{Csg. Annular Capacity} \\ \text{OH Annular Capacity} \\ \text{OH Annular Capacity} \end{array} \right\}$

(d) **820** x **0.006** = **4.92** \div **0.109** (c) = **45** (g) Strokes to displace Choke line

DP/HW x Casing:
Subsea = (b) - (e) \rightarrow DP/HW Length x Casing **6980** x **0.0505** = **352.49** Volume \div **0.109** (c) = **3234** (h) DP/HW x Casing Strokes

Surface = (b) \rightarrow

DP/HW x OH:
(a) - (b) - (f) = DP/HW Length OH **2390** x **0.0459** = **109.70** Volumes

f) DC Length x OH **900** x **0.0292** = **26.28**

= **135.98** Bit to Shoe Volume \div **0.109** (c) = **1248** (i) Bit to Shoe Strokes

(Subsea)
Strokes from bit to surface through choke line:
= (g) + (h) + (i) = **4527**

(Surface Only) Strokes from bit to surface:
= (h) + (i) =

1) *Maximum allowable mud weight before the kick*

$$\text{MAMW} = (\text{LOT pressure} \div 0.052 \div \text{Casing Shoe TVD}) + \text{Test Mud Weight}$$
$$(2725 \div 0.052 \div 7800) + 12.0 = 18.7 \text{ ppg}$$

2) *MAASP before kick*

$$\text{MAASP} = (\text{MAMW ppg} - \text{Current MW ppg}) \times 0.052 \times \text{Casing Shoe TVD}$$
$$(18.7 - 13.5) \times 0.052 \times 7800 = 2109 \text{ psi}$$

3) *Kill mud Weight*

$$13.9 \text{ ppg}$$

4) *Initial Circulating Pressure*

$$750 \text{ psi}$$

5) *Final Circulating Pressure*

$$567 \text{ psi}$$

6) *MAASP after well has been killed*

$$\text{MAASP} = (\text{MAMW ppg} - \text{KMW ppg}) \times 0.052 \times \text{Casing Shoe TVD}$$
$$(18.7 - 13.9) \times 0.052 \times 7800 = 1946 \text{ psi}$$

7) *Dynamic (adjusted) casing pressure after pump start-up*

$$\text{SICP} - \text{Chokeline Friction Pressure}$$

$$600 - 300 = 300 \text{ psi}$$

8) *Pressure drop per step (one-tenth of strokes to Bit)*

18 psi

9) *Pressure drop per 100 strokes from surface to Bit*

$(ICP - FCP) \times 100 \div \text{Strokes from surface to Bit}$

$(750 - 567) \times 100 \div 1724 = 10.6$ (round down to 10 psi)

10) *Strokes from surface to Bit*

1723 strokes

11) *Strokes to displace choke line*

$(\text{Chokeline Length} \times \text{Chokeline Capacity}) \div \text{Pump Output}$

$(820 \times 0.006) \div 0.109 = 45$ strokes

12) *Strokes from bit to surface through choke line*

4527 strokes

13) *Strokes from bit to shoe*

$\text{Open Hole Annular Volume} \div \text{Pump Output}$

$(109.7 + 26.28) \div 0.109 = 1248$ strokes

Subsea Baker #2

Hole Dimensions		
Depth(MD/TVD)	10800	feet
9 ⁵ / ₈ " Casing shoe	8950	feet
Hole size	8 ½	inch
Current mud weight	11.3	ppg
Air gap	70	feet
Water depth	400	feet
Internal Capacities		
6 ½ " Drill collars (length 600 feet)	0.00768	bbbl/foot
5" Drill pipe - capacity	0.01776	bbbl/foot
5" Drill pipe - metal displacement	0.00650	bbbl/foot
5" Drill pipe- closed end displacement	0.02426	bbbl/foot
Choke line	0.006	bbbl/foot
Marine riser	0.39	bbbl/foot
Annular Capacities		
Open hole / Drill collar	0.0292	bbbl/foot
Open hole / Drill pipe	0.0459	bbbl/foot
Casing / Drill pipe	0.0505	bbbl/foot
Riser / Drill pipe	0.3657	bbbl/foot
LOT		
Shoe test mud weight	10.5	ppg
Leak off pressure	1950	psi
Pump Details		
Pump output	0.109	bbbl/stk
SCR pressure up Riser at 40 SPM	450	psi
Choke line friction at 40 SPM	150	psi
Shut in data		
SIDPP	500	psi
SICP	700	psi
Pit gain	15	bbbls

Well Name:
Subsea Baker #2

Date:

Well Info:

- A. Hole TVD
10800
- B. Current MW ppg
11.3
- C. Slow Pump Pressure
450
- D. Slow Pump SPM
40

Kick Info:

- E. (SIDP)
500
- F. (SICP)
700
- G. Pit Gain bbls
15

KWM = (SIDP ÷ .052 ÷ TVD) + Current Mud Weight

$$\left(\frac{\text{(E)}}{\text{(A)}} \div .052 \div \frac{\text{(A)}}{\text{(B)}} \right) + \frac{\text{(B)}}{\text{(B)}} = \text{Round up KWM}$$

$$\left(\frac{500}{10800} \div .052 \div \frac{10800}{11.3} \right) + \frac{11.3}{11.3} = \boxed{12.2}$$

ICP = Slow Pump Pressure + SIDP

$$\frac{\text{(C)}}{\text{(C)}} + \frac{\text{(E)}}{\text{(E)}} = \text{ICP}$$

$$\frac{450}{450} + \frac{500}{500} = \boxed{950}$$

FCP = KWM ÷ CMW x Slow Pump Pressure

$$\frac{\text{(KWM)}}{\text{(B)}} \times \frac{\text{(C)}}{\text{(C)}} = \text{FCP}$$

$$\frac{12.2}{11.3} \times \frac{450}{450} = \boxed{486}$$

Stks to Bit ÷ 10 = **170** stks

Strokes to Bit ▶

	Strokes	Pressure
	0	950
(1)	170	904
(2)	340	858
(3)	510	812
(4)	680	766
(5)	850	720
(6)	1020	674
(7)	1190	628
(8)	1360	582
(9)	1530	536
(10)	1704	486

◀ ICP

46 psi
(ICP - FCP) ÷ 10 =

◀ FCP

Shoe Pressures:

- H. Shoe TVD
8950
- I. LOT Pressure
1950
- J. Test MW
10.5
- K. Frac. Gradient

$$\left(\frac{\text{(I)}}{\text{LOT}} \div .052 \div \frac{\text{(H)}}{\text{Shoe TVD}} \right) + \frac{\text{(J)}}{\text{TMW}} = \text{Round down MAMW}$$

$$\left(\frac{1950}{1950} \div .052 \div \frac{8950}{10.5} \right) + \frac{10.5}{10.5} = \boxed{14.6}$$

Or

Or

$$\frac{\text{Frac. G. (K)}}{\text{Frac. G. (K)}} \div .052 =$$

$$\left(\frac{\text{(MAMW)}}{\text{(MAMW)}} - \frac{\text{(B)}}{\text{CMW}} \times .052 \times \frac{\text{(H)}}{\text{Shoe TVD}} \right) = \frac{1535}{1535} = \text{MASP before kick with Current MW}$$

$$\left(\frac{14.6}{14.6} - \frac{11.3}{11.3} \times .052 \times \frac{8950}{8950} \right) = \frac{1535}{1535}$$

$$\left(\frac{\text{(MAMW)}}{\text{(MAMW)}} - \frac{\text{(KWM)}}{\text{(KWM)}} \times .052 \times \frac{\text{(H)}}{\text{Shoe TVD}} \right) = \frac{1116}{1116} = \text{MASP after kill with Kill MW}$$

$$\left(\frac{14.6}{14.6} - \frac{12.2}{12.2} \times .052 \times \frac{8950}{8950} \right) = \frac{1116}{1116}$$

Volume Info:	Drillstring Volume (surface to bit)	Miscellaneous Calculations:
a) Hole MD 10800	(1) Length (ft) 10200 x Internal Capacity 0.01776 = 181.15 +	Pressure drop per step (one-tenth of strokes to bit): $(ICP - FCP) \div 10 =$ 46
b) Shoe MD 8950	(2) 600 x 0.00768 = 4.61 +	Pressure drop per 100 strokes to bit: $(ICP - FCP) \times 100 \div \text{Strokes to Bit} =$ 27
c) Pump Output (bbls/stk) 0.109	(3) <input type="text"/> x <input type="text"/> = <input type="text"/> +	(Subsea) Dynamic (adjusted) casing pressure after pump start-up: $(SICP - CLF) =$ 550
d) Choke Line Length 470	(4) <input type="text"/> x <input type="text"/> = <input type="text"/> +	
e) Riser Length 470	Total Drillstring Volume 185.76 \div 0.109 (c) = 1704 Strokes Surface to Bit	
f) DC Length 600		

Annular Volumes and Strokes

(Subsea only)

(e) $\left\{ \begin{array}{l} \text{Choke Line Capacity} \\ \text{Choke line} \end{array} \right\}$ (d) **470** x **0.006** = **2.82** \div **0.109** (c) = **26** (g)

DP/HW x Casing:
Subsea = (b) - (e) \rightarrow DP/HW Length x Casing **8480** x **0.0505** = **428.24** Volume \div **0.109** (c) = **3929** (h)
Surface = (b) \rightarrow DP/HW x Casing Strokes

DP/HW x OH:
(a) - (b) - (f) = DP/HW Length OH **1250** x **0.0459** = **57.38** Volumes
+
DC Length x OH (f) **600** x **0.0292** = **17.52**
= **74.9** Bit to Shoe Volume \div **0.109** (c) = **687** (i)

(Subsea)
Strokes from bit to surface through choke line:
= (g) + (h) + (i) = **4642**

(Surface Only) Strokes from bit to surface:
= (h) + (i) =

1) *Maximum allowable mud weight before the kick*

$$\text{MAMW} = (\text{LOT pressure} \div 0.052 \div \text{Casing Shoe TVD}) + \text{Test Mud Weight}$$
$$(1950 \div 0.052 \div 8950) + 10.5 = 14.6 \text{ ppg}$$

2) *MAASP before kick*

$$\text{MAASP} = (\text{MAMW ppg} - \text{Current MW ppg}) \times 0.052 \times \text{Casing Shoe TVD}$$
$$(14.6 - 11.3) \times 0.052 \times 8950 = 1535 \text{ psi}$$

3) *Kill mud Weight*

$$12.2 \text{ ppg}$$

4) *Initial Circulating Pressure*

$$950 \text{ psi}$$

5) *Final Circulating Pressure*

$$486 \text{ psi}$$

6) *MAASP after well has been killed*

$$\text{MAASP} = (\text{MAMW ppg} - \text{KMW ppg}) \times 0.052 \times \text{Casing Shoe TVD}$$
$$(14.6 - 12.2) \times 0.052 \times 8950 = 1116 \text{ psi}$$

7) *Dynamic (adjusted) casing pressure after pump start-up*

SICP – Chokeline Friction Pressure

$$700 - 150 = 550 \text{ psi}$$

8) *Pressure drop per step (one-tenth of strokes to Bit)*

27 psi

9) *Pressure drop per 100 strokes from surface to Bit*

$(ICP - FCP) \times 100 \div \text{Strokes from surface to Bit}$

$(950 - 486) \times 100 \div 1704 = 27 \text{ psi}$

10) *Strokes from surface to Bit*

1704 strokes

11) *Strokes to displace chokeline*

$(\text{Chokeline Length} \times \text{Chokeline Capacity}) \div \text{Pump Output}$

$(470 \times 0.006) \div 0.109 = 26 \text{ strokes}$

12) *Strokes from bit to surface through chokeline*

4642 strokes

13) *Strokes from bit to shoe*

$\text{Open Hole Annular Volume} \div \text{Pump Output}$

$(57.38 + 17.52) \div 0.109 = 687 \text{ strokes}$